

## MOTIVATION

The increasing demand for higher data rates together with the enormous growth of connected devices have pushed standards to adopt larger antenna configurations and higher carrier frequencies, rising the far field distance to thousands of meters, and making it impossible to operate in it due to the high attenuation of such bands. For this reason, near-field models must be taken into account in 5G and beyond.

In this work, we consider a system communicating in the near field and we focus on the coupling caused by the receiver to the transmitter when a massive array is employed in one of the communication system ends. In order to do so, we leverage *multiport communication theory*.

## MULTIPORT COMMUNICATION

Multiport communication theory is a framework that involves a circuit-theoretic approach where the inputs and outputs of a MIMO communication system are associated with ports of a multiport black box, described by its impedance parameters. For the purpose of this work, we consider the (noiseless) simplified system shown in Figure 1.

Defining vectors  $\mathbf{v}_T = (v_{T,1}, \dots, v_{T,N_T})^T$  and  $\mathbf{i}_T = (i_{T,1}, \dots, i_{T,N_T})^T$  (and equivalently for all currents and voltages in the figure), the relationship between the port currents, port voltages and the Z-parameter matrix is:

$$\begin{pmatrix} \mathbf{v}_T \\ \mathbf{v}_R \end{pmatrix} = \begin{pmatrix} \mathbf{Z}_T & \mathbf{Z}_{TR} \\ \mathbf{Z}_{RT} & \mathbf{Z}_R \end{pmatrix} \begin{pmatrix} \mathbf{i}_T \\ \mathbf{i}_R \end{pmatrix}. \quad (1)$$

From circuit analysis, we can obtain the matrix of the (noiseless) input-output relationship  $\mathbf{v}_R = \mathbf{D}\mathbf{v}_G$ :

$$\begin{aligned} \mathbf{D} &= \mathbf{Z}_L(\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R)^{-1}\mathbf{Z}_{RT}(\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T - \mathbf{Z}_{TR}(\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R)^{-1}\mathbf{Z}_{RT})^{-1} \\ &= \mathbf{Z}_L(\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R - \mathbf{Z}_{RT}(\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T)^{-1}\mathbf{Z}_{TR})^{-1}\mathbf{Z}_{RT}(\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T)^{-1}. \end{aligned} \quad (2)$$

In many cases, specially in far-field communications, the *unilateral approximation*  $\mathbf{Z}_{TR} \approx 0$  is used. This assumption simplifies the analysis greatly and leads to the following input-output matrix:

$$\mathbf{D}_{UA} = \mathbf{Z}_L(\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R)^{-1}\mathbf{Z}_{RT}(\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T)^{-1}. \quad (3)$$

This is a coarse approximation. Instead, we propose to verify if the inter-array coupling is much smaller than the intra-array coupling:

$$\|\mathbf{Z}_{TR}(\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R)^{-1}\mathbf{Z}_{RT}\|_F \ll \|\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T\|_F, \quad (4)$$

or equivalently as

$$\|\mathbf{Z}_{RT}(\mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T)^{-1}\mathbf{Z}_{TR}\|_F \ll \|\mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R\|_F, \quad (5)$$

since  $\mathbf{D} \approx \mathbf{D}_{UA}$  in both cases.

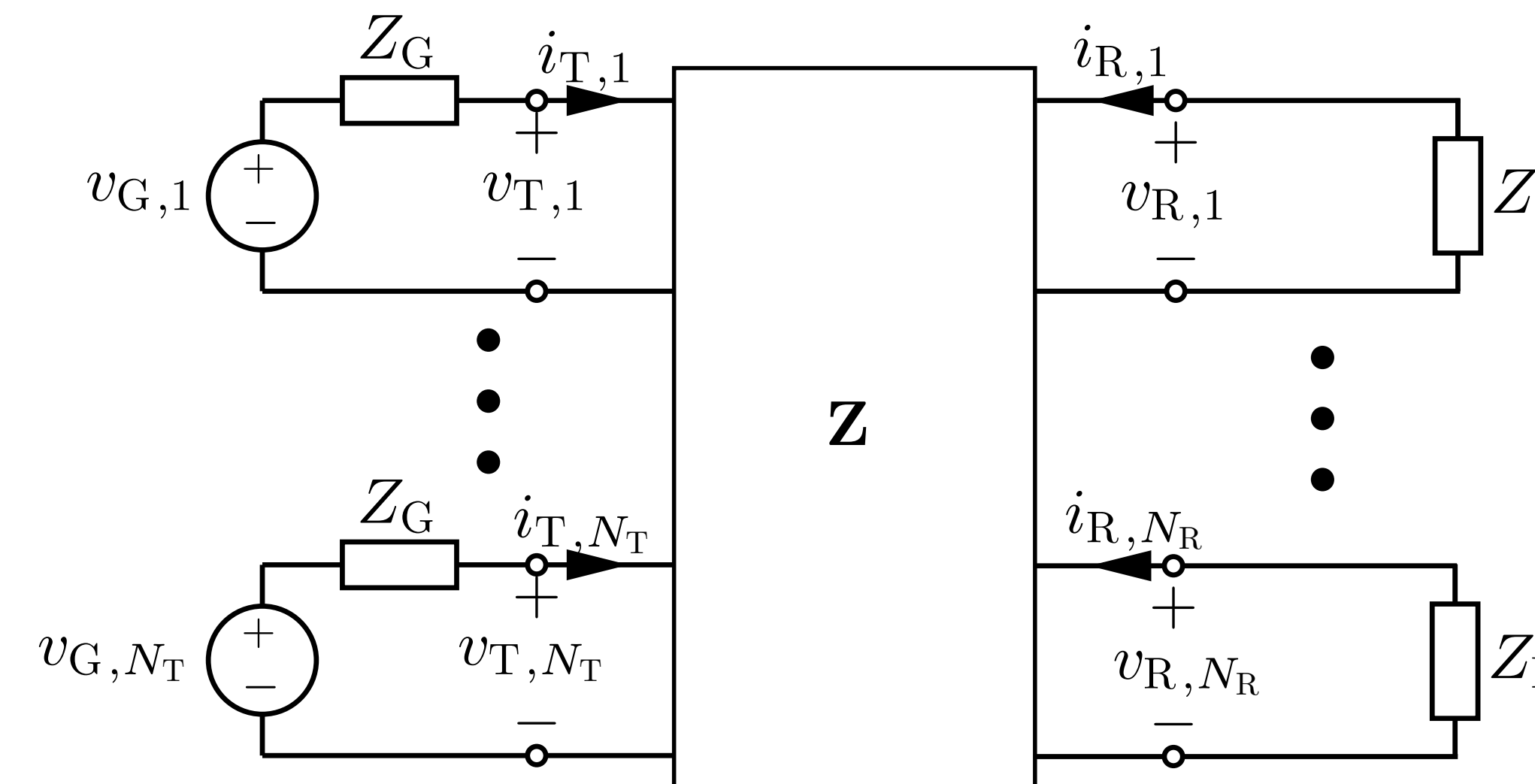


Figure 1. Simplified (noiseless) multiport model of a MIMO system.

## SYSTEM MODEL

Two complementary wireless communication systems are considered: massive MISO with  $N_T = N$  (downlink), and massive SIMO with  $N_R = N$  (uplink). The array is assumed to be a uniform linear array (ULA) with aperture size  $D$  and radiating elements are Hertzian dipoles of length  $l$  with a separation  $d$  between them. The *intra-array coupling* impedance matrix for this setup is:

$$\begin{cases} [\mathbf{Z}]_{m,n} = R_r, & m = n, & 1 \leq m, n \leq N, \\ [\mathbf{Z}]_{m,n} = \frac{3}{2}R_r \cdot j \exp(-jkd|m-n|) \left( \frac{1}{kd|m-n|} - \frac{j}{(kd|m-n|)^2} - \frac{1}{(kd|m-n|)^3} \right), \end{cases} \quad (6)$$

where  $R_r = \frac{2}{3}\pi\eta\left(\frac{l}{\lambda}\right)^2$  is the radiation resistance. Assuming that communication takes place in the *radiative* near field, the Z-parameters of *inter-array coupling* are:

$$[\mathbf{z}_{TR}]_n = jR_r \frac{e^{-jkr_n}}{kr_n}, \quad (7)$$

where  $r_n$  is the distance between the single-antenna device and the  $n$ -th element in the array.

## STUDY OF COUPLING EFFECTS

For MISO and SIMO, conditions (4) and (5) become:

$$\frac{\|\mathbf{z}_{TR}\|_2^2}{|Z_{RL}|} \ll \|\mathbf{Z}_{GT}\|_F, \quad \frac{\|\mathbf{z}_{RT}\|_2^2}{|Z_{GT}|} \ll \|\mathbf{Z}_{RL}\|_F, \quad (8)$$

where  $\mathbf{Z}_{GT} = \mathbf{Z}_G\mathbf{I} + \mathbf{Z}_T$  and  $\mathbf{Z}_{RL} = \mathbf{Z}_L\mathbf{I} + \mathbf{Z}_R$ . Observe that both conditions are equivalent.

Fixing the *inter-element spacing*:

$$\|\mathbf{Z}_{GT}\|_F \sim O(\sqrt{N}), \quad \lim_{N \rightarrow +\infty} \frac{\|\mathbf{z}_{TR}\|_2^2}{|Z_{RL}|} < +\infty, \quad (9)$$

which means that the unilateral approximation is (asymptotically) valid. Numerical results for this scenario are shown in Figure 2.

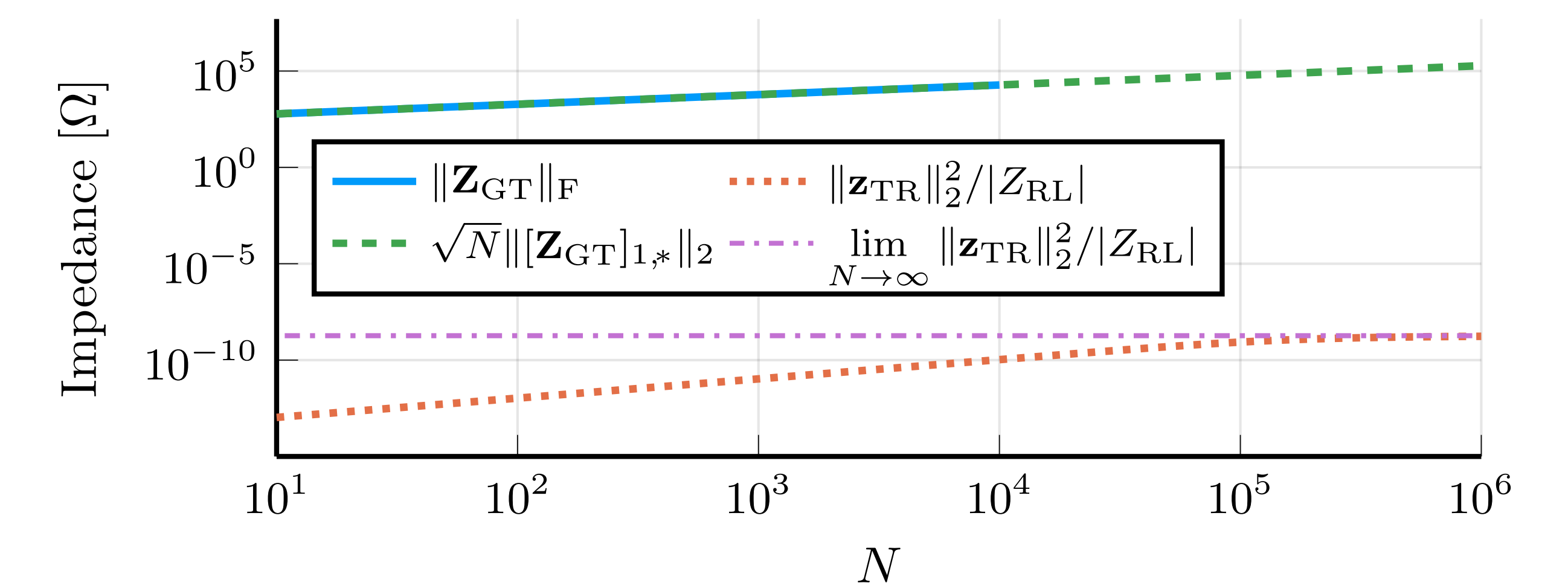


Figure 2. Fixed  $d = \lambda/2$  coupling condition as a function of  $N$  with  $r = 55$  m.

Fixing the *array size* by letting  $d = \frac{D}{N-1}$ ,

$$\|\mathbf{Z}_{GT}\|_F \sim O(N^{3.5}), \quad \|\mathbf{z}_{TR}\|_2^2 \sim O(N). \quad (10)$$

As  $\|\mathbf{Z}_{GT}\|_F$  grows much faster than  $\|\mathbf{z}_{TR}\|_2^2$ , the unilateral approximation is also asymptotically valid when the array size is fixed. The numerical results are shown in Figure 3.

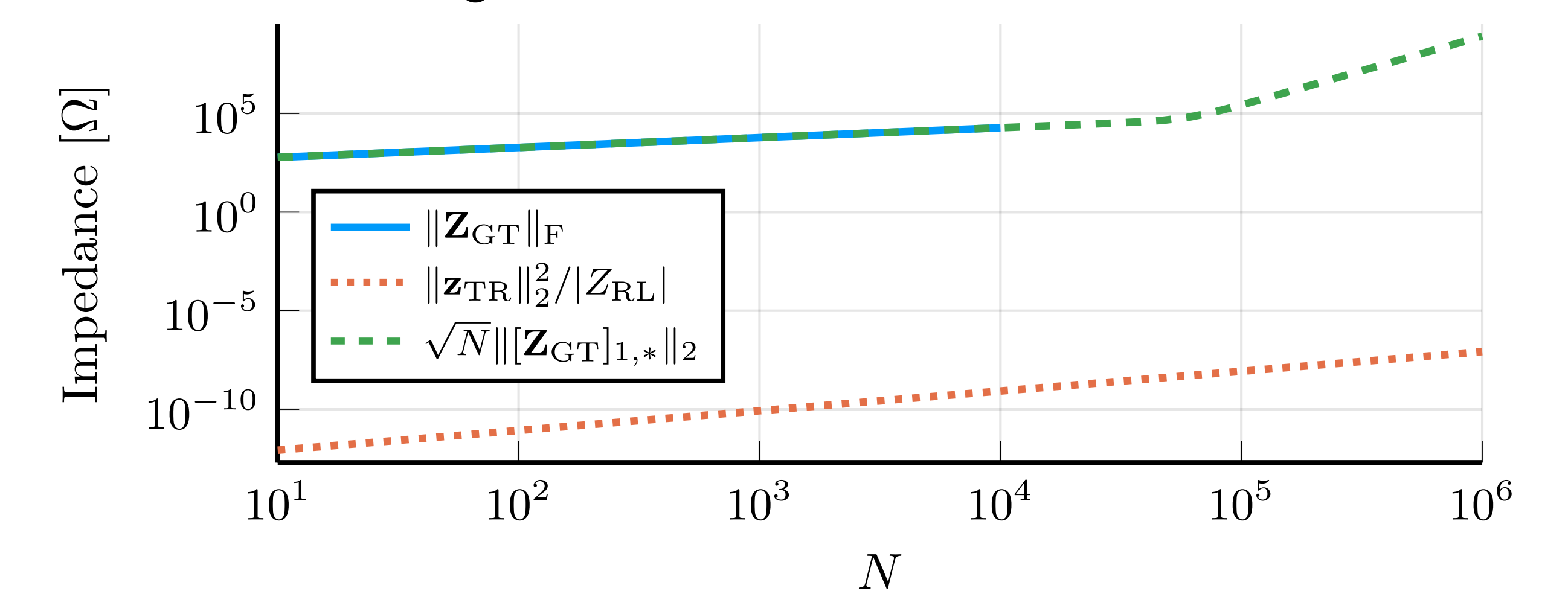


Figure 3. Fixed array size  $D = 1$  m coupling condition as a function of  $N$  with  $r \approx 20$  m.

## REFERENCES

- [1] A. Martí, J. Riba, M. Lamarca, and X. Gràcia, "Asymptotic Analysis of Near-Field Coupling in Massive MISO and Massive SIMO Systems," *IEEE Communications Letters*, 2024. DOI: 10.1109/LCOMM.2024.3416044.

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